

Heat exchanger network design based on physical principles and heuristics
Case 17 – A new benchmark for the 10SP1 literature case

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The 10SP1 example was first presented by Pho and Lapidus in 1973. It comprises five hot and five cold streams and one cold utility. Data are given in Table 17.1.

Table 17.1

Tsupply °C	Ttarget °C	Heat kW	U*f kW/m ² ,K	Description -
160	93	588.93	1.704	H1
249	138	1171.05	1.704	H2
271	149	1532.32	1.704	H3
227	66	2377.97	1.704	H4
199	66	2358.09	1.704	H5
82	177	1641.60	1.704	C1
93	205	1556.80	1.704	C2
38	221	1544.52	1.704	C3
60	160	762.00	1.704	C4
116	222	644.48	1.704	C5
38	82	1878.96	1.704	Cooling

Cold utility = 18.12 EUR/kW,year
 HEX cost formula = 145.63 x Area^{0.60} EUR/year

Composite curves are shown in Figure 17.1.

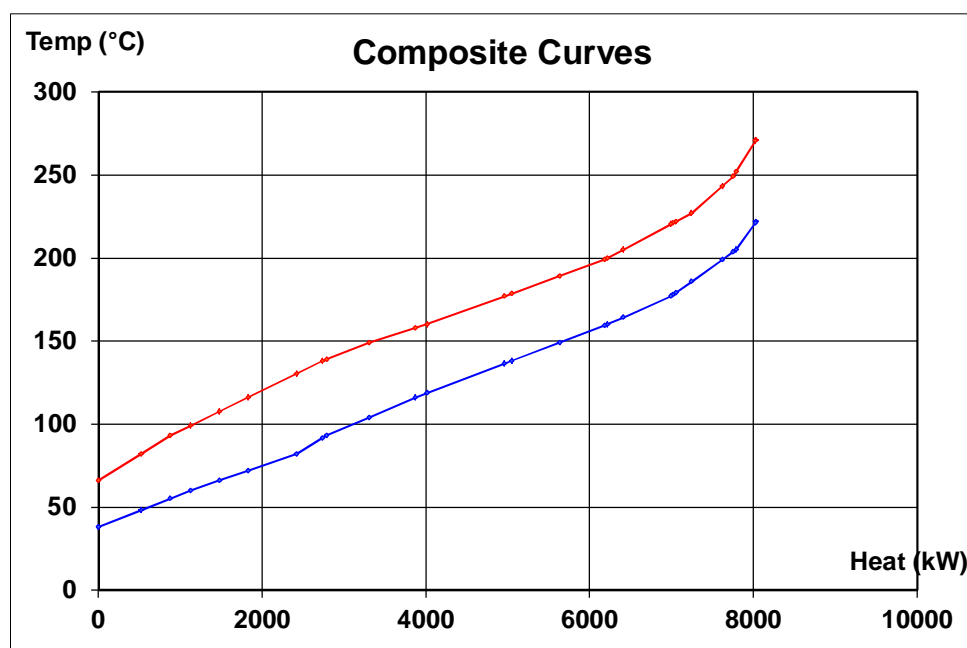


Figure 17.1

The data set leads to a threshold problem with a smallest ΔT of 28 K at the cold side caused by the cold utility. There is, however, also a process pinch with a ΔT of 39.65 K caused by hot stream H5; this becomes more visible in the diagram of the shifted composite curves set up without the cold utility in Figure 17.2.

The area target is 229.18 m², the cost target in the assumption of one single system with 10 units is 43582 EUR.

The curves are nearly parallel over most of the integration range with a ΔT of 40 K to 50 K (Figure 17.3); in view of the design, the problem can be treated as a pinched problem with the pinch for the overall system caused by hot stream H5.

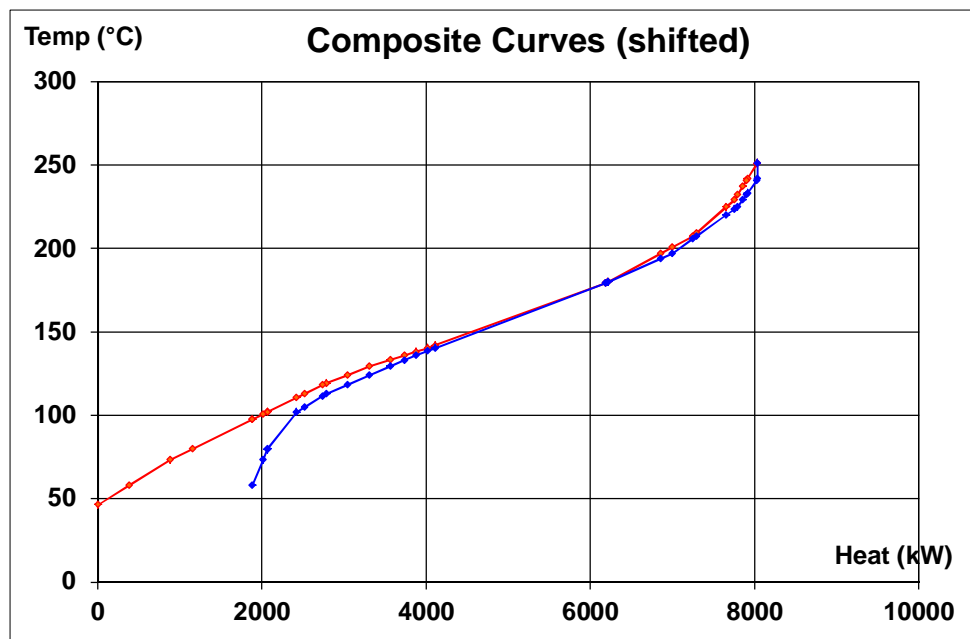


Figure 17.2

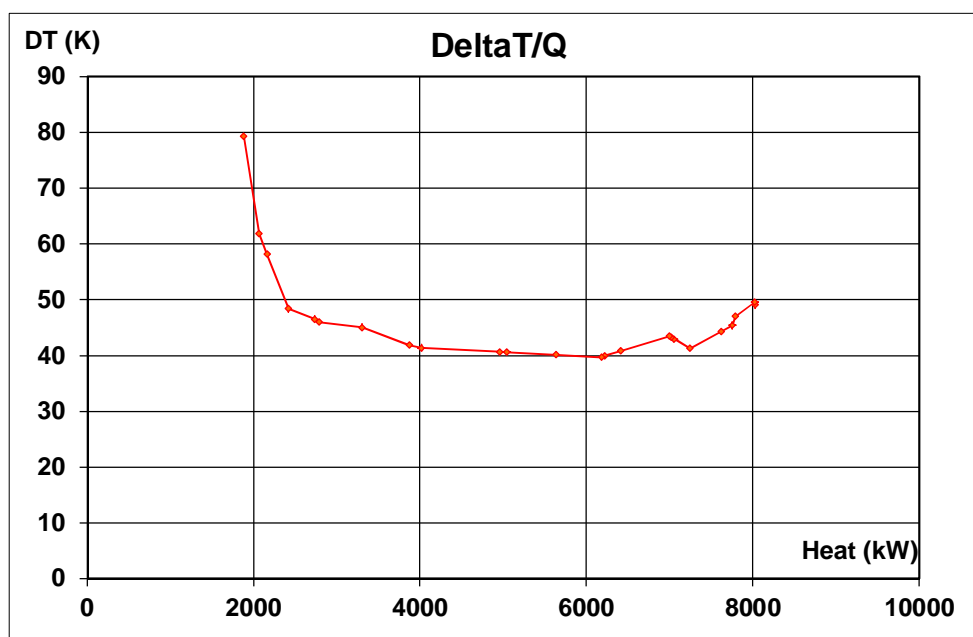


Figure 17.3

The network is developed following pinch design rules in combination with heuristic expert rules based on physical principles rather than on a purely mathematical approach. Analysis of the stream characteristics and of the resulting grid diagram is of primary importance.

The biggest challenge in heat exchanger network synthesis is the complexity related to the size of the problem in combination with the objective of achieving a minimum number of units in view of minimizing cost. If a process stream can be ticked-off at the start, then the complexity of the task is reduced by an order of magnitude.

The process stream with the biggest heat load can never be ticked-off with another process stream; however, it can be a good candidate for ticking-off the biggest counterpart. This leads to the first query:

- Query 1: check whether the biggest hot stream is an appropriate candidate to tick-off the biggest cold stream without violating pinch design rules and vice versa.

Whilst the process stream with the biggest heat load can never be ticked-off itself with another process stream, the likelihood that the process stream with the lowest heat load can be ticked-off is quite high; this leads to the second query:

- Query 2: check whether the smallest (or a small) process stream can be ticked-off without violating pinch design rules

In case of parallel composite curves, the driving force diagram will suggest matches between streams with preferably (almost) equal heat capacity flowrates ($mcp\phi$) in the parallel section; this leads to the third query:

- Query 3: check whether matches are possible between streams with similar $mcp\phi$ in parallel sections of the composite curves.

In view of avoiding stream splitting at the pinch and achieving a minimum number of units, it is advantageous to tick-off streams that are crossing the pinch; this leads to the fourth query:

- Query 4: check whether matches are possible between streams crossing the pinch without violating pinch design rules.

The important pinch design rules to be considered are:

- No heat transfer across the process pinch (or as little as possible);
- Do not give away driving force.

Several matches are possible responding to several queries and also combinations of matches are possible. After accepting one or two or more compatible matches, the remaining problem can be analysed in view of remaining cost and available driving force. The remaining area and cost targets, together with the area and cost already spent on the envisaged matches give a good indication of the final result to be expected, this information can be used to prioritize particular combinations in an early stage, prior to finalizing the integral network. Less attractive combinations can be eliminated in an early stage.

After implementation of the matches, the remaining problem will have been reduced to a manageable number of streams which can easily be solved following a tick-off procedure. The resulting network can be fine-tuned with regard to the stream split ratio, if any, and the ultimate position of the smallest heat exchangers whilst maintaining the main structure of the network.

The procedure leads to results, the best of which are summarized in Table 17.2 and compared with published networks. For networks with stream splits, several networks have been developed that are better than the best published. For networks without stream split, the two best networks published so far were also identified.

The networks mentioned in Table 17.2 are shown in Figure 17.4 through Figure 17.13.

Table 17.2

Cases	First matches	Area (m ²)	Cost ('000)	Splits
Original data set - targeting				
		229.18	43.582	
With stream splits				
Case 1	H2-C2 & H4-C1	242.24	43.316	2
Case 2	H2-C4 & H4-C1	239.88	43.324	1
Case 3	H2-C4 & H4-C2	250.39	43.328	1
Case 4	H2-C3 & H4-C1	244.74	43.338	1
Case 5	H2-C3 & H4-C2	251.02	43.349	1
Without stream splits				
Case 6	H2-C3 & H4-C1	246.95	43.393 (1)	0
Case 7	H2-C3 & H4-C2	260.61	43.411 (2)	0
Case 8	H2-C3 & H5-C1	260.20	43.437	0
Case 9	H2-C3 & H3-C5 & H4-C2	252.93	43.450	0
Case 10	H2-C3 & H3-C2 & H4-C5	266.62	43.611	0
Published results				
Lin & Miller (2004)			43.329	4
Pettersson (2008)			43.331	3
Gupta, Ghosh (2010)			43.342	1
Huang, Karimi (2013)			43.359	1
Zhao, Yin, Huo (2013)			43.429	1
Flower & Linnhoff (1978)			43.934	0
Papoulias, Grossmann (1983)			43.934	0
Lewin et al. (1998)			43.752	0
Pariyani et al. (2006)			43.439	0
Yerramsetty, Murty (2008)			43.538	0
(1) He, Cui (2013)			43.393	0
(2) Peng, Cui (2015)			43.411	0

U*f H = 3.50
 T_{Hot} = 377.0

Heating
 Cooling 1878.96

Area 242.24 m²
 # HEX 10

Cost
 Energy Capital 34.047
 Total 43.316

U*f C = 1.704
 T_{in} = 38.0
 T_{out} = 82.0

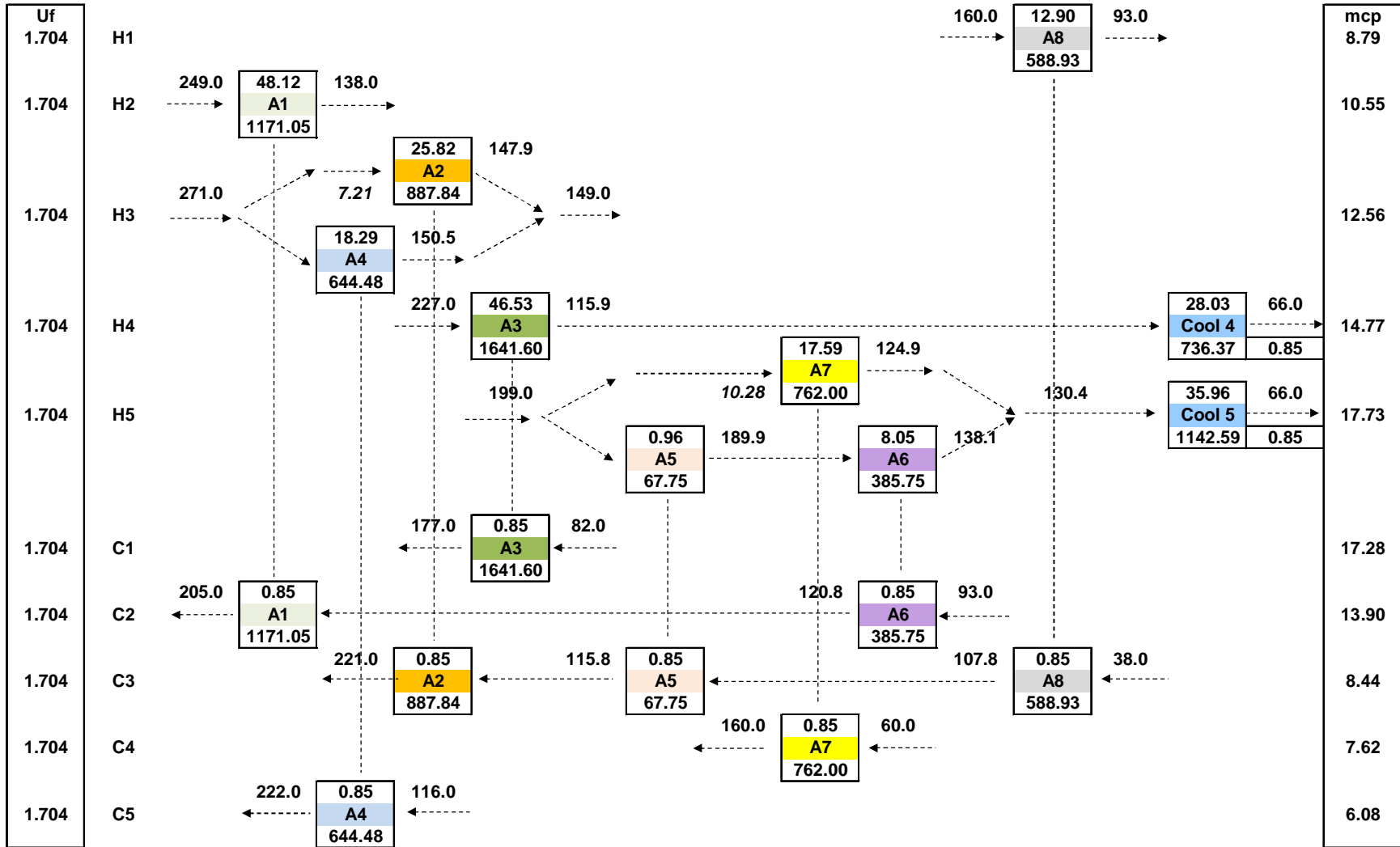


Figure 17.4

U*f H = 3.50
 THot = 377.0

Heating
 Cooling 1878.96

Area 239.88 m²
 # HEX 10

Cost Energy 34.047
 Capital 9.277
 Total 43.324

U*f C = 1.704
 Tin = 38.0
 Tout = 82.0

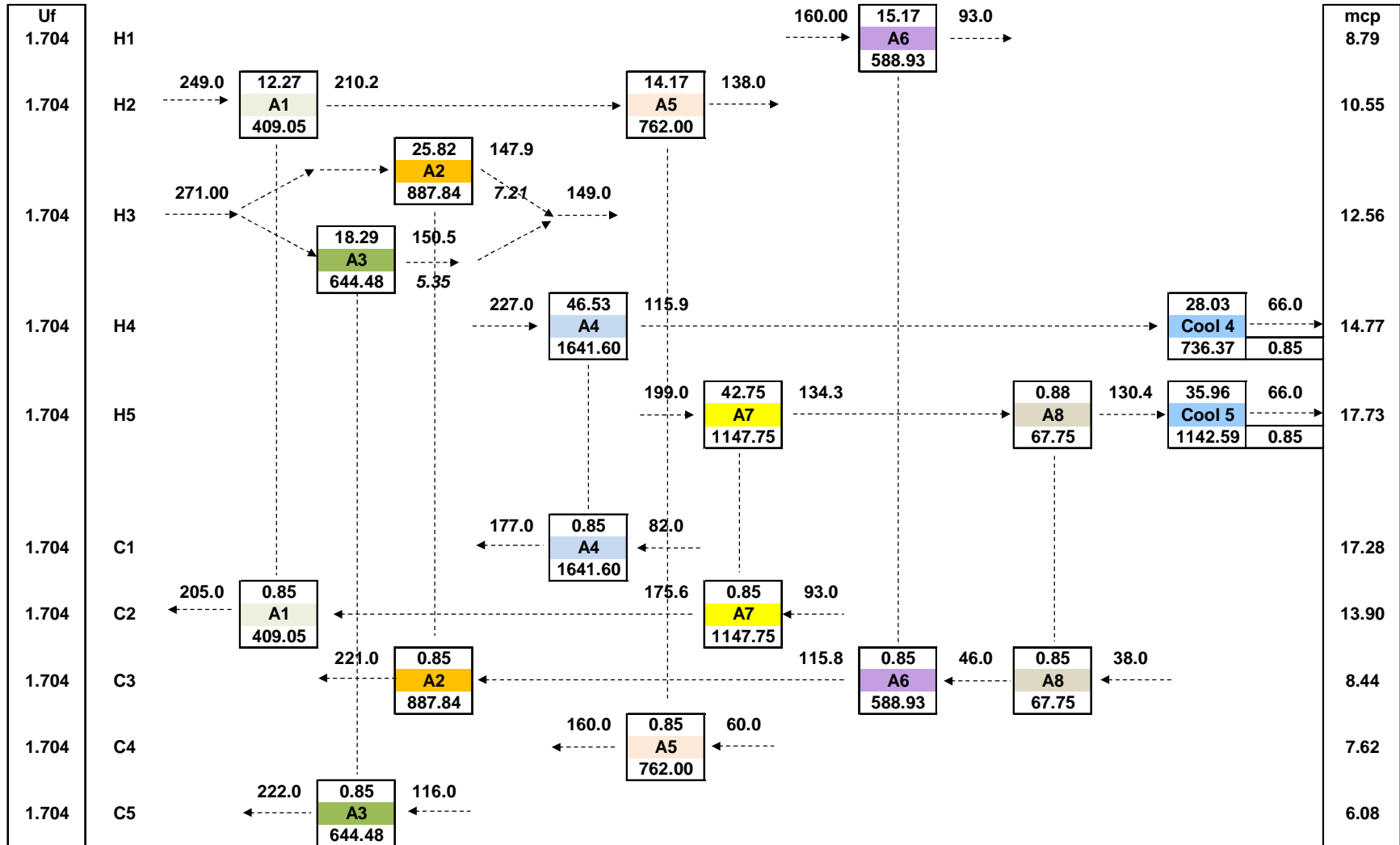


Figure 17.5

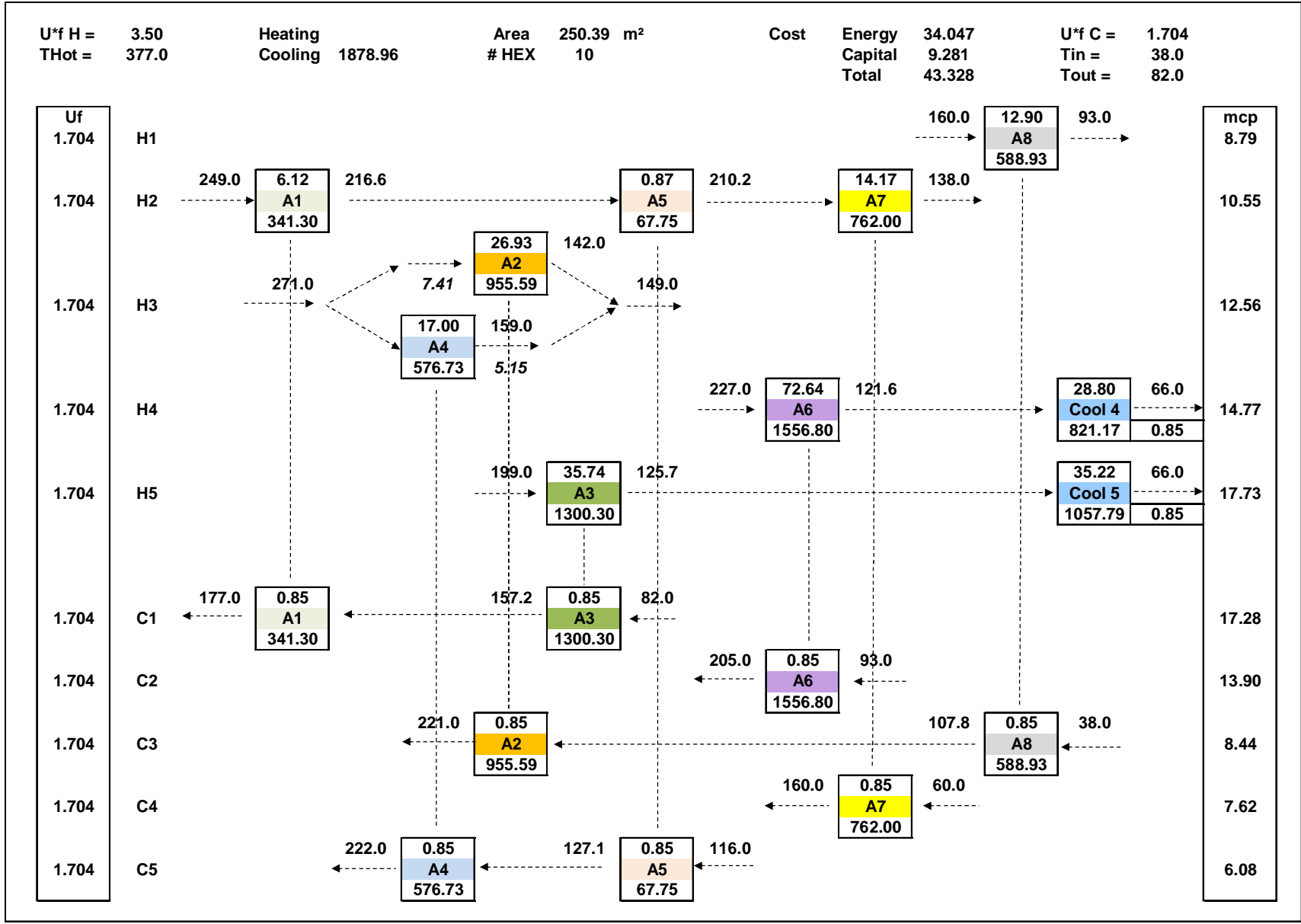


Figure 17.6

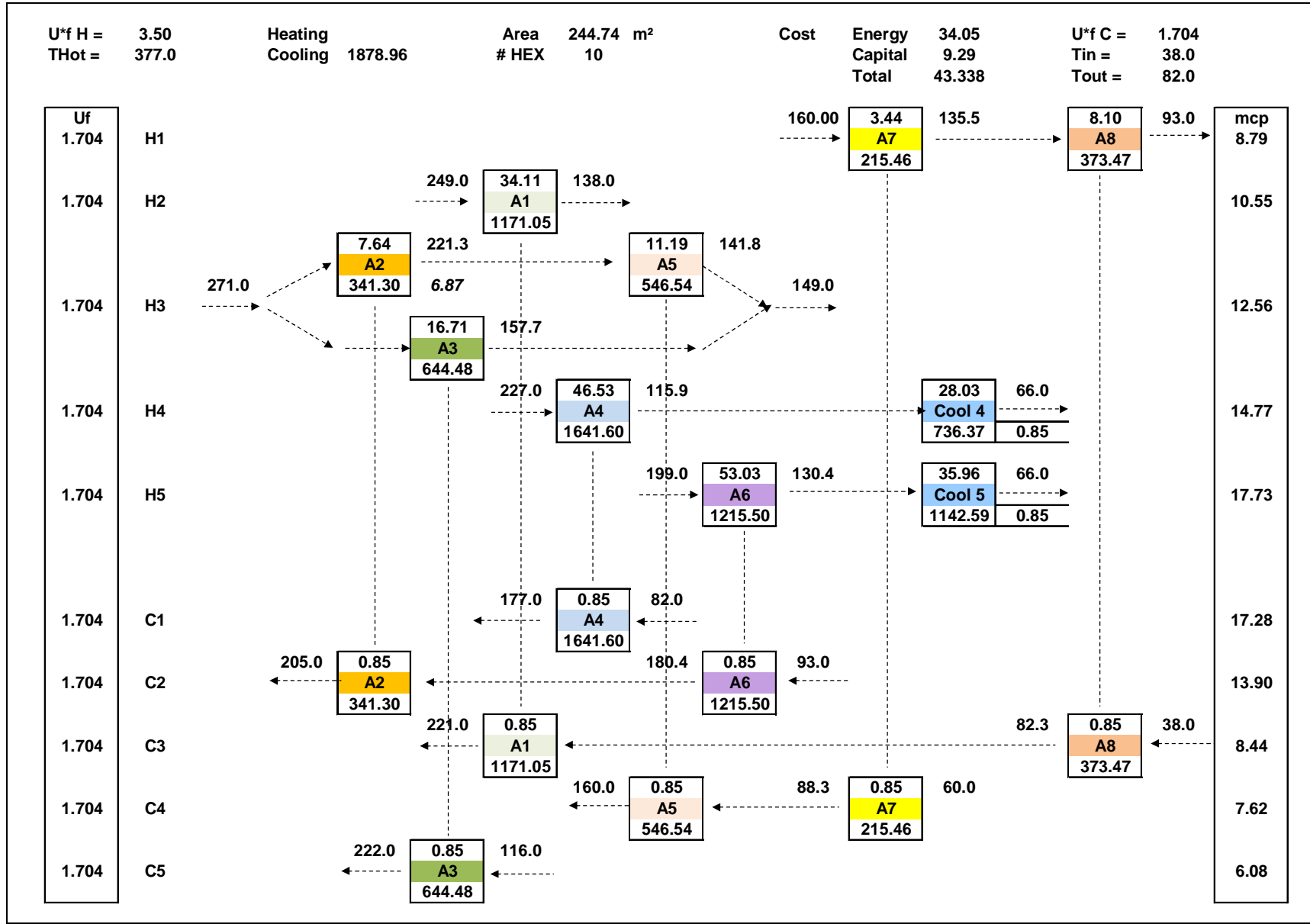


Figure 17.7

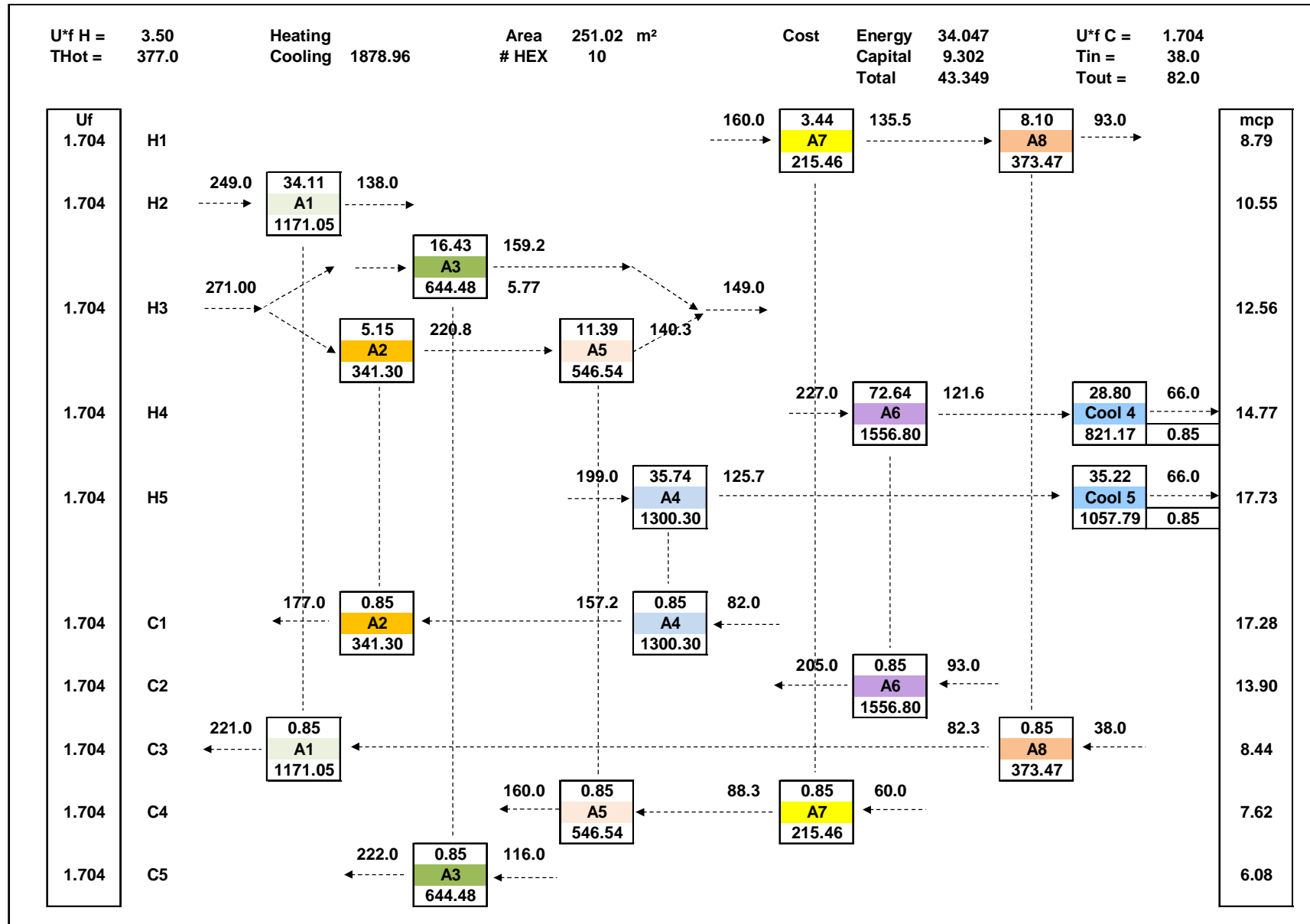


Figure 17.8

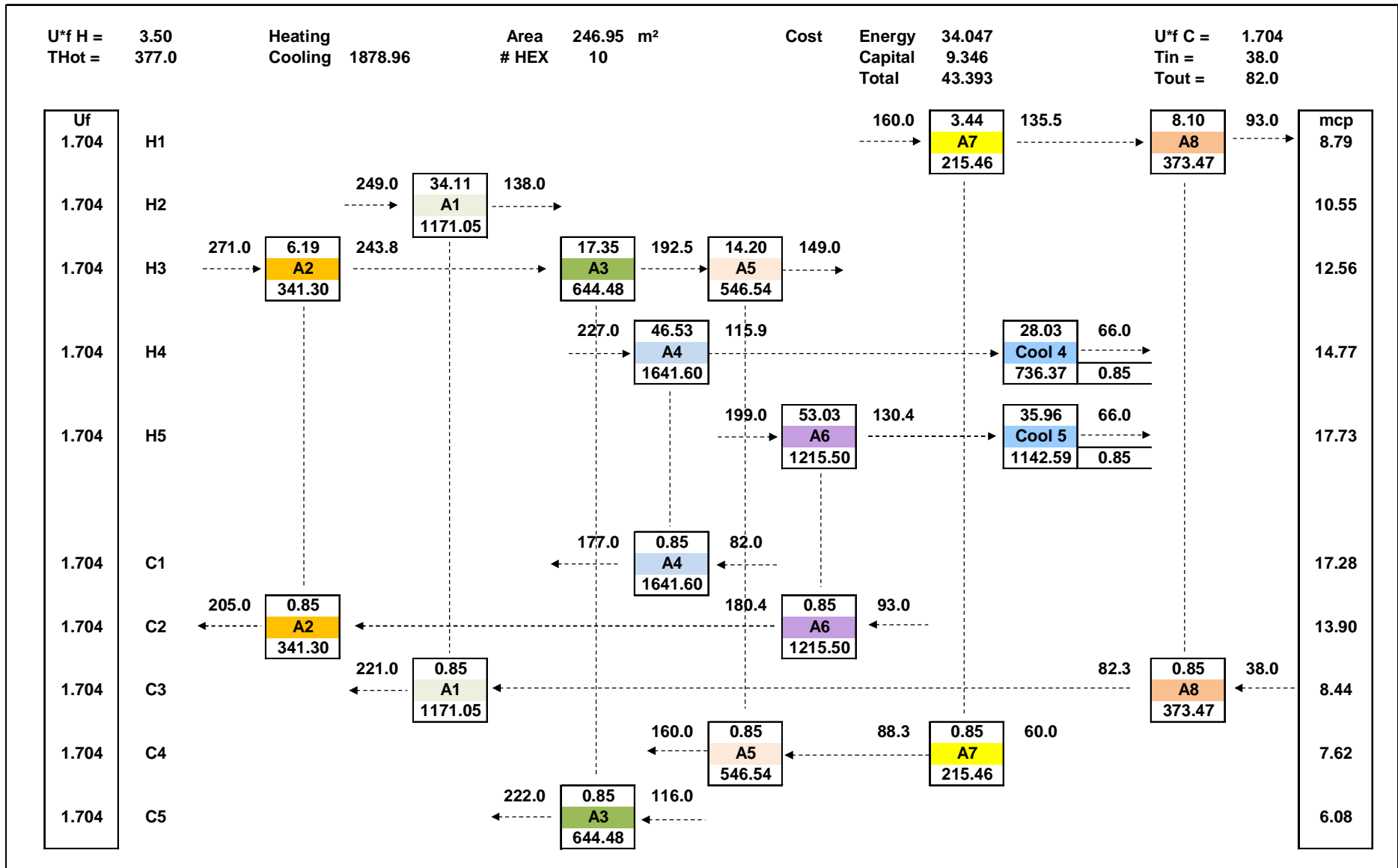


Figure 17.9

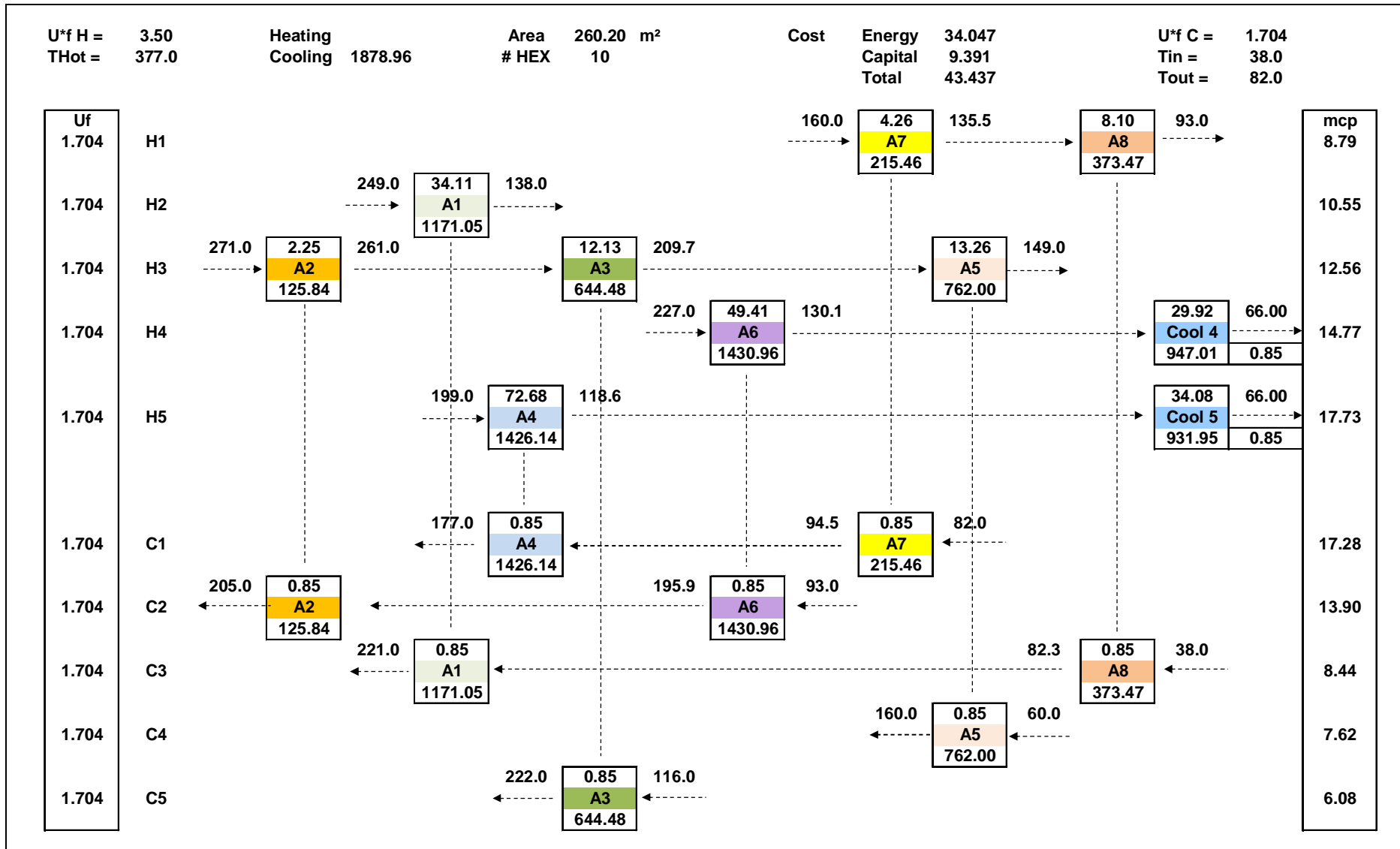


Figure 17.11

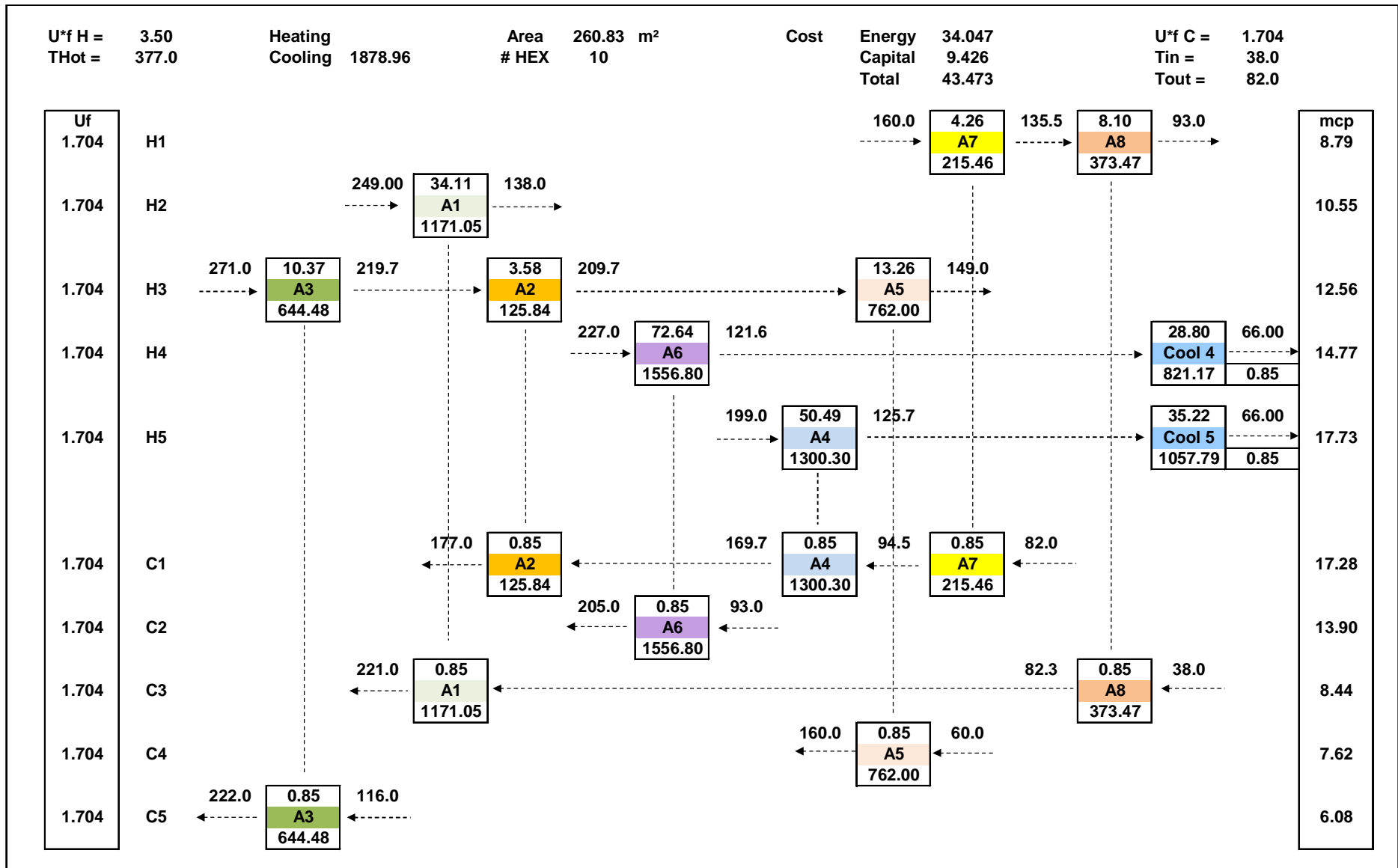


Figure 17.12

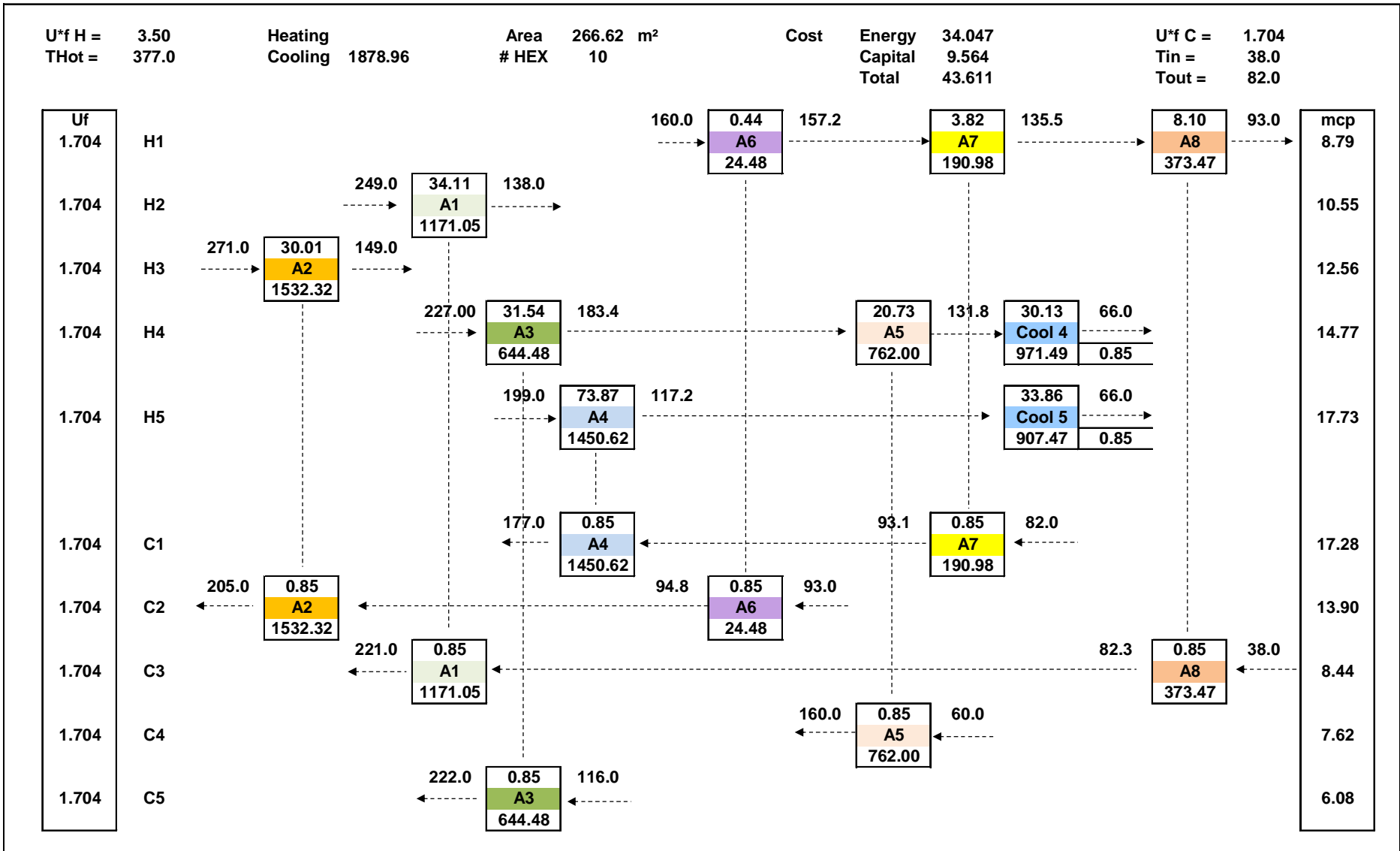


Figure 17.13